

# Relationship between oxidation, stresses, morphology, local resistivity, and optical properties of TiO<sub>2</sub>, Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub> thin films on SiC

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**Abstract.** The relationship between internal mechanical stresses, surface morphology, nanoscale electrical properties, and optical characteristics in TiO<sub>2</sub>, Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>, and SiO<sub>2</sub> thin films on SiC substrates was investigated. The oxide films were synthesized using the rapid thermal annealing and analyzed through scanning spreading resistance microscopy, photoluminescence, and absorption spectroscopy. Tensile stresses were found in the films, they are attributed to thermal and lattice mismatch, oxidation, and grain boundaries. These stresses influence on surface morphology, resistivity variations, and photoluminescence intensity. Surface roughness and grain structure were found to correlate with variations in resistivity, which were attributed to conductive pathways along grain boundaries and possible metallic phases. Photoluminescence intensity was also observed to correlate with estimated lattice mismatch strain. Gd<sub>2</sub>O<sub>3</sub>/SiC exhibited the fewest defects, while Er<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> showed more, with Er<sub>2</sub>O<sub>3</sub> being the most mismatched and roughest. The results indicate that internal strains in oxide thin films on SiC substrates can influence on surface morphology, leading to formation of defects and spatial inhomogeneity. These fluctuations in local conductivity and luminescence center density have significant implications for dielectric and optical applications. The study provides insights for future processing refinements to mitigate internal strains and enhance the performance of oxide thin films in semiconductor and optical technologies.

**Keywords:** TiO<sub>2</sub>, Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>, stresses, oxide/semiconductor structures, absorption, photoluminescence, scanning spreading resistance microscopy.

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## 1. Introduction

Oxide/semiconductor (OS) structures are one of the most demanded functional elements of semiconductor electronics. OS structures are used to create photoresistors, dynamic memory elements, as a gate in field-effect transistors, *etc.* The quality of interface in these structures largely defines the performance of metal-dielectric-semiconductor (MIS) structures [1–15]. Also, oxide films are widely used for optical coatings, protective coatings, in photocatalysis, gas sensors, biocompatible coatings, *etc.* [16–19]. OS structures are commonly applied in electronic technology, where silicon or silicon carbide are used as semiconductors, and silicon oxide usually acts as a traditional oxide in these structures. However, recently, in the structures oxide/SiC(Si), oxides of titanium [1–5] and rare earth elements (REE) [7–10], the so-called alternative dielectrics (dielectrics with high permittivity – high-*k*

dielectrics), are considered as oxides [11–15]. In addition to a high value of dielectric permittivity and band gap width, these oxides have high transparency in the visible spectral range, chemical and thermal stability [20, 21].

The optical, mechanical, and electrical characteristics of the oxide film/SiC structure are affected by both the microscopic nature of the surface relief and the mechanical stresses arising in the structure. The inhomogeneous spatial distribution of interfacial states at the oxide film/SiC interface, due to different local electronic structures for different SiC crystallographic directions, or with different configurational environments of impurity atoms (often nitrogen), can cause a non-uniform distribution of electrical properties caused by spatial fluctuations of the surface potential [6]. For example, in the work [22] it was shown that in SiO<sub>2</sub> films on a silicon carbide substrate owing to different values of internal mechanical stresses at the SiO<sub>2</sub>/SiC interface for the films grown by various methods, a shift in the

maximum of the PL spectrum is observed. A slight change in the position of PL band maximum for the samples with different ways for creation of the thin SiO<sub>2</sub> film is a consequence of the redistribution of defects localized at the SiO<sub>2</sub>/SiC interface with a change in the internal mechanical strains value at the SiO<sub>2</sub>/SiC interface [22].

The main reasons for the occurrence of internal strains in the oxide film/substrate structures are as follows: 1) the difference in the coefficients of thermal expansion of the film and substrate, leading to the appearance of thermal stresses; 2) mismatch between the crystal lattices of the film and substrate, resulting in mismatch strains; 3) the presence of internal strains due to phase inhomogeneities and structural defects in the material of the film and substrate.

The oxidation process involves several physical phenomena, including the diffusion of oxygen atoms into the metal film, the reaction of oxygen with metal atoms to form metal oxide, and the migration of metal and oxide ions. The rate of these processes can be influenced by such factors as annealing temperature and time, oxygen pressure, and the properties of the original metal film. For instance, a higher annealing temperature can increase the diffusion rate and reaction rate, leading to more complete oxidation. However, it could also introduce more defects due to the increased mobility of atoms. The volume change associated with the oxidation reaction is another stress source, inducing compressive stress in the film. The magnitude of these stresses can influence the density and type of defects in the film, namely: dislocations, vacancies and grain boundaries, which can, in turn, affect the film electrical and optical properties.

Since REE oxides are usually synthesized at lower temperatures than SiO<sub>2</sub> oxide, it can be expected that the films based on REE oxides will not cause significant mechanical stresses at the REE oxide/semiconductor substrate interface. At the same time, for oxides of titanium and rare-earth elements, the impact of mismatched stresses on the properties of the OP structure, where silicon carbide acts as a semiconductor, will be much higher than that for the SiO<sub>2</sub>/SiC structure. There is still a lack of published information regarding the local homogeneity of these REE oxide films and how it affects the physical properties of thin-film structures.

The aim of this work is to evaluate internal mechanical stresses and to analyze their influence on nanomorphology and local resistive properties of the surface, as well as their relationship with the optical characteristics of TiO<sub>2</sub>(Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>)/SiC thin oxide film structures in comparison with SiO<sub>2</sub>/SiC structures.

## 2. Samples and research methods

Metal oxide films were synthesized using the rapid thermal annealing (RTA) of titanium, erbium, and gadolinium metal films deposited on SiC substrates *via* thermal sputtering. The RTA oxidation was performed at 350 °C in oxygen atmosphere.

The surface nanomorphology and the corresponding local distributions of the film specific resistivity were studied using scanning spreading resistance microscopy (SSRM) with a NanoScope IIIa Dimension 3000TM scanning probe microscope [6, 23–25]. Platinum probes with a nominal tip radius of 20 nm were used. The bias voltage did not exceed 5 V. The optical properties of the structures were characterized on the basis of the transmission and photoluminescence (PL) spectra. Absorption and PL spectra were recorded using the SDL-2 setup within the range  $\lambda = 400 \dots 800$  nm. A SIRSh-200 spectral lamp was used as a continuous spectrum source for measuring the transmission spectra. Nitrogen laser radiation ( $\lambda_{ex} = 337$  nm) was used to excite the PL spectra. All the optical measurements were carried out at room temperature.

## 3. Comparative evaluation of mechanical stresses in oxide film/SiC structures

To estimate the total mechanical stress, we systematically analyzed each of the strain components and their relative magnitude by using the common models of thin film mechanics. The stresses can be additive or partially relaxed due to plastic deformation. The total stress  $\sigma$  in a thin film that is formed on a thick substrate is expressed using the formula  $\sigma = E_f \varepsilon_{tot}$ , where  $E_f$  is the film elastic modulus and  $\varepsilon_{tot}$  is the total strain. The total strain has components  $\varepsilon_{tot} = \varepsilon_{th} + \varepsilon_{lm} + \varepsilon_{ox} + \varepsilon_{gb}$ , where  $\varepsilon_{th}$ ,  $\varepsilon_{lm}$ ,  $\varepsilon_{ox}$ ,  $\varepsilon_{gb}$  are the thermal mismatch, lattice mismatch, oxidation and grain boundary stresses, respectively. The oxidation and grain boundary stresses represent the internal strains due to the phase inhomogeneities and structural defects [26, 27].

The most common consideration for thin film structures is biaxial deformation. The biaxial stress state implies stresses parallel ( $\sigma_{||}$ ) and perpendicular ( $\sigma_{\perp}$ ) to the film plane. In our estimations, we assume coherent stresses ( $\sigma_{||} = \sigma_{\perp}$ ),  $\sigma_{||} = E_f / (1 - \nu) \varepsilon_{tot}$  where  $\nu$  is the Poisson ratio for the film. However, it should be noted that if the film relaxes, the strain may become non-equi-biaxial.

The thermal strain between the film and substrate is  $\varepsilon_{th} = (\alpha_f - \alpha_s) \Delta T$ , where  $\alpha_f$ ,  $\alpha_s$  refer to the thermal expansion coefficients of the film and substrate, respectively [28].  $\Delta T$  is the difference in temperature between the stress-free deposition temperature and the observation temperature. The intrinsic misfit strain between the film and substrate due to lattice parameter mismatch is  $\varepsilon_{lm} = (a_f - a_s) / a_s$ , where  $a_f$ ,  $a_s$  are the lattice parameters [28]. In the course of oxidation process, the molar volume increases due to incorporation of oxygen according to the expression  $\Delta V/V = (M_f - M_i) / (\rho M_i)$ , where  $M_f$  and  $M_i$  are the molar masses per unit volume before and after oxidation, and  $\rho$  is the density of the oxidized film. It is the origin of oxidation strain  $\varepsilon_{ox}$ . Finally, for a nanocrystalline film,

**Table 1.** Data used for the estimates of mechanical stresses in TiO<sub>2</sub>(Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>)/SiC structures. Lattice parameters (*a*, *c*), thermal expansion coefficient ( $\alpha_{f,s}$ ), Poisson's ratio ( $\nu_f$ ), elastic modulus ( $E_{f,s}$ ), film thickness ( $d_{f,s}$ ) and  $\beta$  – grain boundary free energy per unit area.

	<i>a</i> , nm	<i>c</i> , nm	$\alpha_{f,s} \times 10^6 \text{ }^\circ\text{C}^{-1}$	$\nu_f$	$E_{f,s}$ , GPa	$\beta$ , J/m <sup>2</sup>	$d_{f,s}$ , nm
SiC	0.309	1.05(4H) 1.51(6H)	~3 [29]	0.16	392	1.5	~500·10 <sup>3</sup>
TiO <sub>2</sub>	0.459[30]	0.295 [30]	8.3 [30]	0.32 [30]	244 [30]	0.60	~65 [32]
Gd <sub>2</sub> O <sub>3</sub>	0.376[30]	0.589 [30]	10 [30]	0.26 [30]	150 [30]	0.75	~70 [32]
Er <sub>2</sub> O <sub>3</sub>	1.005[30]		10.5 [30]	0.338 [31]	177 [31]	0.87	~150 [32]
SiO <sub>2</sub>	0.491	0.540	~0.5 [30]	0.17 [30]	71 [30]	0.35	~70 nm [22]

**Table 2.** Estimates of mechanical stresses in TiO<sub>2</sub>(Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>)/SiC structures: thermal ( $\sigma_{th}$ ), lattice mismatch ( $\sigma_{lm}$ ), oxidation stress ( $\sigma_{ox}$ ) and grain boundary stress ( $\sigma_{gb}$ ). Typical stress values for similar structures as observed experimentally ( $\sigma$ ).

	$\sigma_{th}$ , GPa	$\sigma_{lm}$ , GPa	$\sigma_{ox}$ , GPa	$\sigma_{gb}$ , GPa	$\sigma$ , GPa
TiO <sub>2</sub>	0.62	0.523	61	0.003	0.65 tensile [33–35]
Gd <sub>2</sub> O <sub>3</sub>	0.46	0.13	36	0.003	0.60 tensile [36, 37]
Er <sub>2</sub> O <sub>3</sub>	0.65	1.8	39	0.003	0.70 tensile [38]
SiO <sub>2</sub>	–0.24	0.15	37	0.007	0.30 tensile [34, 35, 39]

additional strain can develop due to grain boundary formation. The common model for grain boundary strain is  $\varepsilon_{gb} = \beta / (E_f D)$ , where  $\beta$  is the grain boundary free energy per unit area,  $D$  is the grain size, and  $\varepsilon_{gb}$  represents the dilatational misfit.

Since the investigated films contain amorphous phase and are polycrystalline rather than single crystal oriented, we cannot simply use the lattice mismatch formula for  $\varepsilon_{lm}$ , assuming direct epitaxial lattice matching. Inaccuracies in analyzing the lattice contribution to strain can be minimized by considering various factors, such as the distribution of grain orientations in the film relatively to the SiC substrate, the impact of lattice rotation and alignment between grains in the film and SiC surface, as well as the average coherent lattice matching strain over different orientations. Assuming hexagonal closed packed structure, there are mainly two types of grain orientations – basal plane parallel to substrate (*c*-axis normal) and prismatic plane parallel (*c*-axis in plane). The basal orientation exhibits lower lattice mismatch strain because of the better fit between closely-packed planes. The prismatic orientation results in greater mismatch, caused by the alignment of open lattice planes with the substrate. The effective averaged lattice mismatch strain was estimated using the predominance of basally oriented grains.

Simple volume conservation arguments of the Pilling–Bedworth type are obviously insufficient in themselves, but experimental trends suggest that some volume conservation principle may be involved as a starting point [28]. Estimating grain boundary energies for oxides without specific experimental data is also challenging. In materials science, it is a widely accepted principle that the grain boundary energy is related to the surface energy of the material. It has been observed that in many materials, the grain boundary energy is roughly 50% of the surface energy. These values were used in our estimations.

The data used for estimating the results of the above-described evaluations are summarized in Tables 1 and 2.

The obtained results of estimating the stresses in SiO<sub>2</sub>(TiO<sub>2</sub>, Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>)/SiC structures showed that in all cases these strains are tensile; moreover, the minimum strain values can be expected in SiO<sub>2</sub> and Gd<sub>2</sub>O<sub>3</sub> films. The maximum strain value is predicted for Er<sub>2</sub>O<sub>3</sub> films (see Table 2). It should be noted that the granular structure of the films (grain boundaries) will make a minimal contribution to the integral strains of the structure. In this case, the ratio of the nanocrystalline and amorphous phases in films should be taken into account, which, in turn, will also affect the level of misfit strains.

It is assumed that the thermal strains in the films of Ti, Er, and Gd metals deposited on a silicon carbide substrate to form an oxide layer by treatment in oxygen will be approximately equal. In this case, silicon oxide films are special due to the opposite sign of thermal strain. As for the  $\text{Er}_2\text{O}_3$  films, when texturing the granular structure of these films, one should expect a significant increase in misfit strains. The level of these strains can be an order of magnitude higher than those in  $\text{Gd}_2\text{O}_3$  films. For  $\text{TiO}_2$  films, one should expect an increased susceptibility to the quality of oxidation, since the increase in bulk strain of the oxide phase is almost two times higher than the values for other films under consideration. It is important to note that the provided values were used for a rough comparison of the factors that influence the level of mechanical stress in thin films, and this was done using the very basic models for estimation purposes. The actual stress values in films are influenced by a multitude of factors including the specifics of films formation, their structural characteristics and the relaxation processes involved. Stress values reported in the literature for analogous structures exhibit substantial variation, with reported values spanning from several hundred megapascals to a few gigapascals.

#### 4. Experimental results and discussion

As shown in [32], in all cases the surface of Er, Ti, Gd oxide films on a silicon carbide substrate is inhomogeneous in phase composition and has an island character. As the oxidation time increases, the island density increases. In this case, the  $\text{TiO}_2$  oxide film retains a granular texture, while the  $\text{Gd}_2\text{O}_3$  and  $\text{Er}_2\text{O}_3$  films start to exhibit surface grain aggregation as oxidation time progresses. One result of this granular surface in oxide films is a nonuniform distribution of conductivity across the films, among other effects.

Fig. 1 presents the data obtained from scanning spreading resistance microscopy (SSRM) for  $\text{TiO}_2/\text{SiC}$  and  $\text{Er}_2\text{O}_3/\text{SiC}$  structures. Additionally, Fig. 1 includes SSRM data for  $\text{SiO}_2/\text{SiC}$  structures, which were obtained through thermal oxidation at a temperature of 1150 °C, for comparison.

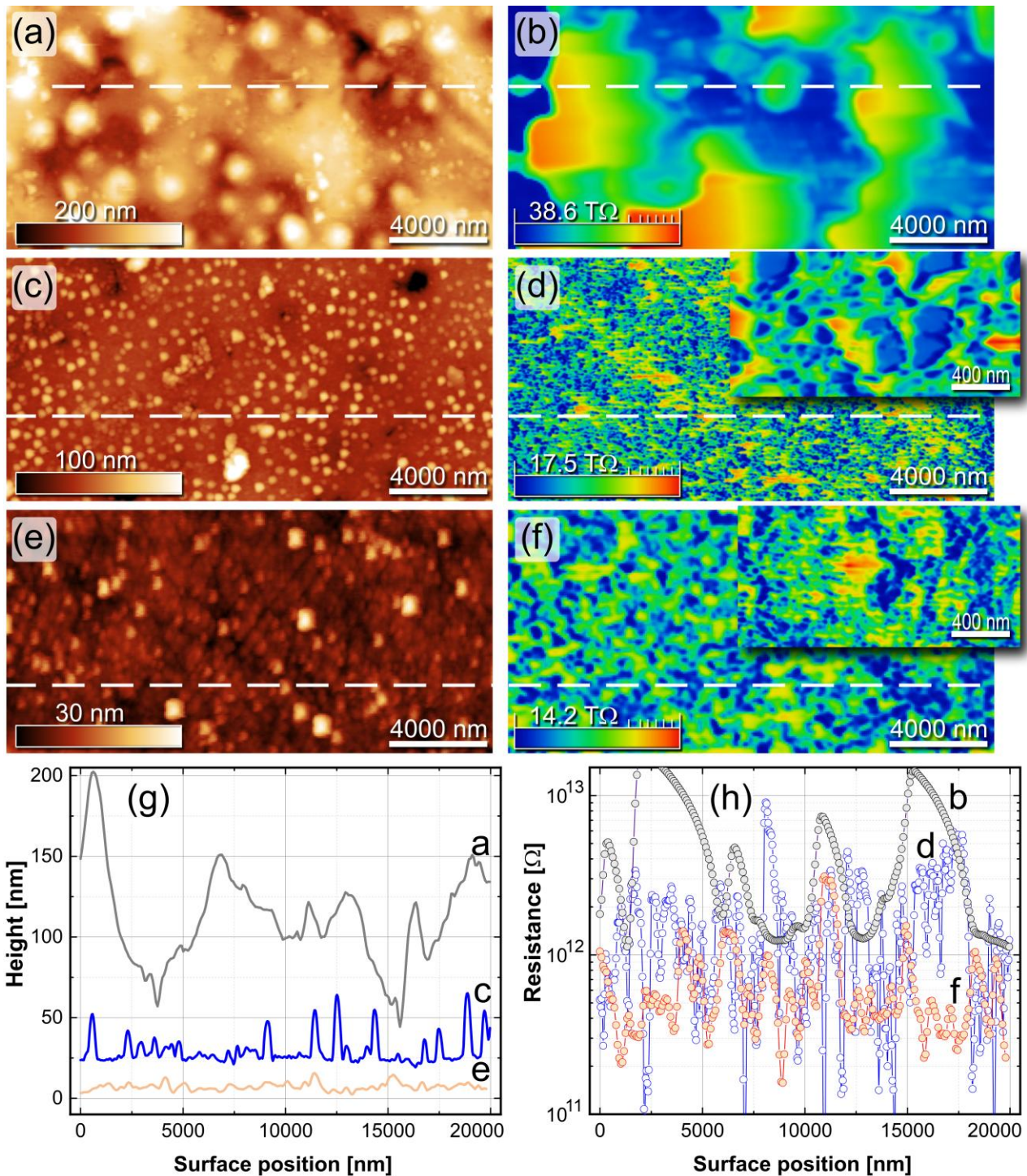
One advantage of the SSRM method is its ability to monitor physicochemical processes in surface layers by identifying changes in local electrophysical properties. The high sensitivity of this technique, which measures resistances ranging from  $10^2$  to  $10^{14}$  Ohm, enables the detection of alterations in the concentration and mobility of charge carriers in surface layers. These alterations are associated, in part, with the influence of mechanical stresses on defect formation processes on the oxide surface. The resistivity of the films, as determined by SSRM, offers insight into the electrical properties of the film associated with carrier mobility and concentration, and can be related to these physical processes and the structural integrity of the films.

The  $\text{Er}_2\text{O}_3$  film displays a nanocrystalline grain structure (Fig. 1a), but with a more uniform grain size distribution around 200...300 nm (Figs 1a, 1g, curve *a*). This is evident in the relatively smooth granular morphology of the surface. The larger 34 nm surface roughness arises from sporadic growth of large 1500 nm diameter hillocks on the surface. These are seeded by defects that initiate uncontrolled precipitation, reflecting spatial inhomogeneity in structural perfection. Concerning to  $\text{TiO}_2$ , the submicron-scale regions of lower resistivity result from interrelated transport along grain boundaries and oxygen vacancies. The polycrystalline structure with random grain orientations creates discontinuities along the grain boundaries, which concentrates current. The large hillocks likely act as localized current leakage channels due to high defect densities. This enables resistivity reduction to extend over longer scales as compared to the other films. In addition, the annealing temperature close to 350 °C may result in incomplete oxidation of the full 150 nm Er layer. Metallic Er has much higher conductivity than  $\text{Er}_2\text{O}_3$ , so any unoxidized metallic Er regions along grain boundaries would further reduce local resistivity. Overall, the polycrystalline structure and high surface roughness creates low resistivity paths on the scale of 1 to 5  $\mu\text{m}$  vertically in the  $\text{Er}_2\text{O}_3$  film. As can be seen from the SSRM data,  $\text{Er}_2\text{O}_3$  films are characterized by the maximum value surface-averaged local resistivity – 50 MOhm-cm (Figs 1b, 1h, curve *a*).

The  $\text{TiO}_2$  film likely has a nanocrystalline structure, leading to more pronounced variation in the local resistivity (Figs 1c, 1g, curve *c*). The  $\text{TiO}_2$  film has a sufficiently higher roughness of 11 nm, indicating a textured surface and relatively larger grains (150...300 nm). This higher roughness suggests that the film has a higher density of surface defects, which can be attributed to the high mechanical stresses and low homogeneity of  $\text{TiO}_2$  film.

The three-fold higher thermal expansion coefficient of  $\text{TiO}_2$  as compared to that of SiC produces a compressive stress around 0.6 GPa during cooling. This high stress can cause incomplete oxidation and residual metallic Ti grains or regions along grain boundaries. Metallic Ti has resistivity orders of magnitude lower than  $\text{TiO}_2$ . Overall, the nanocrystalline structure and high compressive stress in  $\text{TiO}_2$  leads to local resistivity variations on the scale of the grain size, around 50...300 nm (Figs 1c, 1g, curve *c*). The overall resistivity of the  $\text{TiO}_2$  film is 10 MOhm-cm, which is significantly less than the resistivity of the  $\text{Er}_2\text{O}_3$  films (Figs 1d, 1h, curves *a, b*).

The  $\text{SiO}_2$  film has the lowest roughness of 3 nm, which indicates a relatively smooth surface (Figs 1e, 1g, curve *e*). This low roughness suggests that the film has a low density of surface defects such as hillocks and voids, which can be attributed to the low thermal expansion mismatch between  $\text{SiO}_2$  and SiC as well as the low intrinsic strain in the  $\text{SiO}_2$  film. The  $\text{SiO}_2$  film on SiC is



**Fig. 1.** Related SSRM height and resistance maps for  $\text{Er}_2\text{O}_3$  (a, b),  $\text{TiO}_2$  (c, d) and  $\text{SiO}_2$  (e, f) films. Corresponding cross-sections of the maps along the dashed lines are shown in (g, h).

expected to be amorphous and have the relatively uniform resistivity, with only small localized regions of lower resistivity. This is because  $\text{SiO}_2$  readily forms a stable amorphous oxide during thermal deposition. The amorphous structure lacks grain boundaries or defects that could lead to localized current pathways.

The resistivity of  $\text{SiO}_2$  film is 6 MOhm-cm, which is less than that of titanium oxide films and significantly less than that of erbium oxide films (Fig. 1h). It suggests that the film has a low density of defects, namely: vacancies and dislocations. However, the thermal oxidation process can result in some non-uniformity and

non-stoichiometric  $\text{SiO}_x$  regions, if oxidation is incomplete. Any residual unoxidized Si or  $\text{SiO}_x$  will have higher conductivity than  $\text{SiO}_2$ . But since oxidation rates of SiC are relatively rapid, these regions are expected to be small, less than 60 nm in size. This reflects the local resistance SSRM map and the corresponding cross-section (Figs 1f, 1h, curve f).

As can be seen from Fig. 1, the surface morphology of the thin films, as reflected in their roughness and grain size, is closely related to the local resistivity of the films, *i.e.* homogeneity (Fig. 1). The roughness and grain size can be influenced by the stress in the film and the physical processes during oxidation. For instance, high stress can lead to a rougher surface and larger grains, as the film seeks to minimize the stress by forming a more relaxed grain structure. This can increase the resistivity, since grain boundaries can act as barriers to electron transport, thereby increasing the scattering of electrons and hence the resistivity.

On the other hand, a smoother surface and smaller grains, as in the case of the  $\text{SiO}_2$  film, can lead to lower resistivity. The smoother surface reduces the scattering of

electrons at the surface, while the smaller grains increase the density of grain boundaries, which can act as pathways for electron transport, thereby reducing the resistivity.

Fig. 2a shows the absorption spectra of  $\text{TiO}_2(\text{Gd}_2\text{O}_3, \text{Er}_2\text{O}_3)$  structures in the transparency region of the SiC substrate ( $E_{g, \text{SiC}} = 3.2 \text{ eV}$ ). When analyzing the transmission and photoluminescence spectra of the analyzed structures, it should be taken into account that these spectra are an integral characteristic of the structure, as in the case of  $\text{SiO}_2/\text{SiC}$  structures [22]. Therefore, in the absorption spectra of samples, their absorption edge is defined by the structure component that has the smallest band gap. In this case, such a structural element is a silicon carbide substrate (see Table 1). The relatively low concentrations of impurity atoms both in the oxide film and in the substrate (in particular, impurities of boron and nitrogen typical for silicon carbide [40]) are evidenced by the absence of individual absorption bands in the transmission spectrum of the oxide film/silicon carbide structures (Fig. 2a).

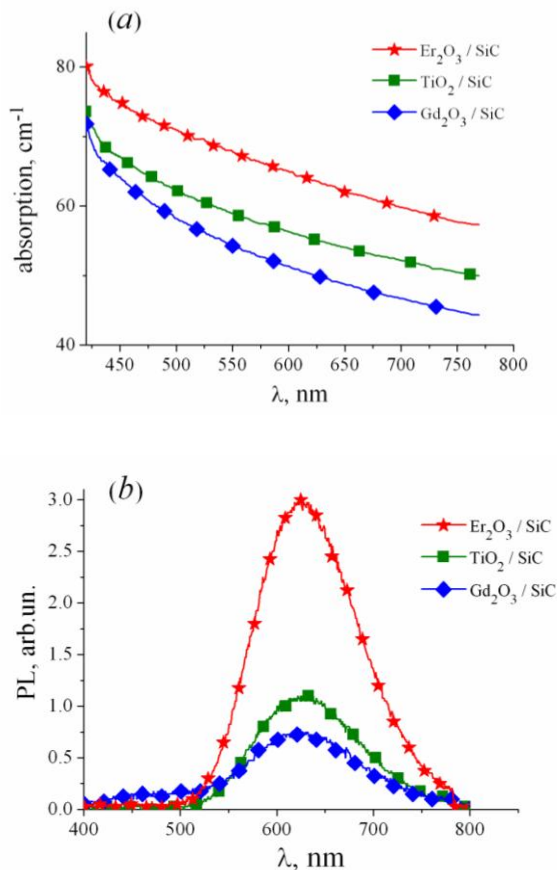
The characteristic features of the luminescence spectra of the oxide film/substrate structure (Fig. 2b) are also determined by several factors: the PL spectrum of the metal oxide film itself, the degree of transparency of the metal oxide film both in the excitation radiation region and in the silicon carbide luminescence region, and is an integral PL spectrum of proper film and silicon carbide.

Fig. 2b shows the photoluminescence spectra of the  $\text{TiO}_2(\text{Gd}_2\text{O}_3, \text{Er}_2\text{O}_3)/\text{SiC}$  heterostructures (PL was excited from the side of the oxide film). A comparative analysis of the PL spectra measured from the side of the metal oxide film and from the side of silicon carbide showed that the spectral composition of the PL band of the metal oxide film/silicon carbide structure is mainly caused by the contribution of silicon carbide. The absence of bands characteristic of the PL of REE oxides in the PL spectra can be explained by the fact that the PL intensity of silicon carbide significantly exceeds the PL intensity of thin films of REE oxides.

The observed SiC PL band with a maximum at 630 nm is associated in the literature [40–42] with radiative transitions in the centers impurity (nitrogen) – defect or impurity – vacancy (usually, the carbon vacancy is considered). In the earlier work [43], this band was associated with recombination processes caused by the presence of defects near the surface of a silicon carbide crystal.

As can be seen from Fig. 2, there is a correlation between the absorption and PL spectra of the  $\text{TiO}_2(\text{Gd}_2\text{O}_3, \text{Er}_2\text{O}_3)/\text{SiC}$  structures: with an increase in the absorption coefficient, the PL intensity increases.

It should be noted that  $\text{TiO}_2$ ,  $\text{Gd}_2\text{O}_3$  and  $\text{Er}_2\text{O}_3$  oxide films were obtained at the same temperature. At the same time, a change in the method of forming the thin  $\text{SiO}_2$  film on the surface of silicon carbide, which was accompanied, among other things, by a change in the



**Fig. 2.** Absorption spectra in the transparency range of the SiC substrate ( $E_{g, \text{SiC}} = 3.2 \text{ eV}$ ) (a), and PL spectra ( $\lambda_{\text{exc}} = 337 \text{ nm}$ ,  $h\nu_{\text{exc}} \approx 3.68 \text{ eV}$ ) (b) of  $\text{TiO}_2(\text{Gd}_2\text{O}_3, \text{Er}_2\text{O}_3)/\text{SiC}$  structures. The PL spectrum of the SiC substrate without an oxide film was used as a reference to compare the PL spectra.

temperature of obtaining the oxide, led to a change in the position of the maximum of the PL band for samples with different methods of forming a thin film [22]. In this case, the optical absorption spectra of the SiO<sub>2</sub>/SiC structures almost coincided [22].

Structural disordering caused by the mismatch of crystal lattices in the PL spectra is reflected by the change in PL characteristics of the upper silicon carbide layer adjacent to the oxide film/SiC interface. The energy position and normalized shape of the PL lines completely coincide for the structures TiO<sub>2</sub>(Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>)/SiC. At the same time, the PL intensity in the Gd<sub>2</sub>O<sub>3</sub>/SiC structures is almost 1.5 times lower than in the TiO<sub>2</sub>/SiC structures and 4 times lower than in the Er<sub>2</sub>O<sub>3</sub>/SiC structures. It means that at room temperature, in the Er<sub>2</sub>O<sub>3</sub>/SiC and TiO<sub>2</sub>/SiC structures, in contrast to the Gd<sub>2</sub>O<sub>3</sub>/SiC structures, there is a significant concentration of radiative recombination centers.

As can be seen from Fig. 2, the observed changes in the PL intensity and in the absorption coefficient of the TiO<sub>2</sub> (Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>)/SiC structures correlate with the value of  $\sigma_f$  – misfit strain (see Table 2). Thus, the maximum PL intensity (~3 arb. units) and the maximum values of the absorption coefficient (~63 cm<sup>-1</sup> for  $\lambda = 630$  nm) are observed for the Er<sub>2</sub>O<sub>3</sub>/SiC structures, for which the value of misfit stresses is maximum (see Table 2). In this case, additional defects, which are PL centers, may appear at the Er<sub>2</sub>O<sub>3</sub>/SiC interface. At the same time, the Gd<sub>2</sub>O<sub>3</sub>/SiC interface is characterized by a minimum amount of defects caused by misfit stresses in the oxide film/substrate structures (see Table 2). In this case, the PL intensity at the maximum of the band for the Gd<sub>2</sub>O<sub>3</sub>/SiC structures is ~0.73 arb. un., and the value of the absorption coefficient for  $\lambda = 630$  nm is ~50 cm<sup>-1</sup>. For TiO<sub>2</sub>/SiC structures, an intermediate situation is observed: at misfit stresses (see Table 2), the PL intensity at the band maximum for TiO<sub>2</sub>/SiC structures is ~1.1 arb. un., and the value of the absorption coefficient for  $\lambda = 630$  nm is ~55 cm<sup>-1</sup>.

## 5. Conclusions

This study elucidated the interrelations between internal mechanical strains, surface morphology, nano-scale electrical properties, and optical characteristics in TiO<sub>2</sub>, Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>, and SiO<sub>2</sub> thin films on SiC substrates. The oxide films were synthesized *via* rapid thermal annealing and analyzed using scanning spreading resistance microscopy, photoluminescence and absorption spectroscopy. Estimations of strain components revealed net tensile stresses arising from thermal mismatch, lattice mismatch, oxidation, and grain boundaries. Scanning spreading resistance microscopy demonstrated that surface roughness and grain structure correlated with spatial variations in resistivity, attributed to conductive pathways along boundaries and possible metallic phases. Photoluminescence intensity has also been found to correlate with estimated lattice mismatch strain.

Gd<sub>2</sub>O<sub>3</sub>/SiC has exhibited the least amount of defects, while Er<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> have shown a higher amount, with Er<sub>2</sub>O<sub>3</sub> being most mismatched and roughest. The appearance of PL centers of a different nature, as was observed in the SiO<sub>2</sub>/SiC structures [22], was not seen in the TiO<sub>2</sub> (Gd<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>)/SiC structures. These results demonstrate that internal strains in oxide thin films on SiC substrates can influence surface morphology, leading to formation of defects and spatial inhomogeneity. The associated fluctuations in local conductivity and density of luminescence centers have important implications for both dielectric and optical applications.

Overall, this work reveals the multiscale connections between film stresses, nanoscale electrical and optical properties, as well as ultimate thin film performance. These insights pave the way for future processing refinements to mitigate internal strains in order to improve the functionality of oxide thin films for both semiconductor and optical technologies.

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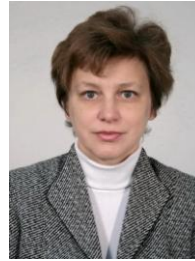
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### Взаємозв'язок між окисненням, напруженням, морфологією, локальним опором та оптичними властивостями тонких плівок $\text{TiO}_2$ , $\text{Gd}_2\text{O}_3$ , $\text{Er}_2\text{O}_3$ , $\text{SiO}_2$ на $\text{SiC}$

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Досліджено взаємозв'язок між внутрішніми механічними напруженнями, морфологією поверхні, нанорозмірними електричними властивостями та оптичними характеристиками в тонких плівках  $\text{TiO}_2$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  та  $\text{SiO}_2$  на підкладках  $\text{SiC}$ . Оксидні плівки були синтезовані з використанням швидкого термічного відпалу та проаналізовані за допомогою скануючої мікроскопії опору розтікання, фотолюмінесценції та спектроскопії поглинання. У плівках були виявлені напруження, що розтягують, які пов'язані з термічною невідповідністю та невідповідністю кристалічних ґраток плівки та підкладки, окисненням і межами зерен. Ці напруження впливають на морфологію поверхні, зміни питомого опору та інтенсивності фотолюмінесценції. Було виявлено, що шорсткість поверхні та структура зерен корелюють зі змінами питомого опору, які пояснюються провідними шляхами вздовж меж зерен та можливими металевими фазами. Було також виявлено, що інтенсивність фотолюмінесценції корелює з передбачуваною деформацією невідповідності ґраток.  $\text{Gd}_2\text{O}_3/\text{SiC}$  показав найменшу кількість дефектів, у той час як  $\text{Er}_2\text{O}_3$  і  $\text{TiO}_2$  показали більшу кількість дефектів, причому  $\text{Er}_2\text{O}_3$  виявився найбільш неузгодженим і найшорсткішим. Результати показують, що внутрішні напруження в тонких оксидних плівках на підкладках  $\text{SiC}$  можуть впливати на морфологію поверхні, що призводить до утворення дефектів та просторової неоднорідності. Ці флуктуації локальної провідності та щільності центрів люмінесценції мають велике значення для діелектричних та оптичних застосувань. Дослідження дає уявлення про майбутні удосконалення обробки для зниження внутрішніх напружень та підвищення продуктивності виготовлення тонких оксидних плівок у напівпровідникових та оптичних технологіях.

**Ключові слова:**  $\text{TiO}_2$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$ , напруження, оксид/напівпровідникові структури, поглинання, фотолюмінесценція, скануюча мікроскопія опору розтікання.